

## **Halcrow MWT**

Queensland Curtis LNG Project EIS  
Microsimulation Assessment

**16 April 2009**



**QGC - A BG Group Business**

***Halcrow***

# QGC - A BG Group Business



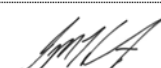
## Queensland Curtis LNG Project EIS

### Microsimulation Assessment

## Contents Amendment Record

This report has been issued and amended as follows:

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# 1 Introduction

## 1.1 Background

Halcrow Pacific Pty Ltd (trading as Halcrow MWT) was commissioned by QGC - A BG Group Business (QCG) to undertake a microsimulation assessment for the Environmental Impact Statement (EIS) of the proposed Queensland Curtis LNG (QCLNG) Project ('the Project'). The Project includes the development of existing coal seam gas fields in the Surat Basin of western Queensland, the construction of a liquefied natural gas (LNG) processing and export facility on Curtis Island near Gladstone in central Queensland and the construction of a pipeline network linking the gas fields to the processing and export facility.

The coverage of this study relates exclusively to the Project's LNG processing and exporting facility. This report is to be read in conjunction with the Road Impact Assessment (the 'RIA'), *Queensland Curtis LNG Project EIS Traffic and Transport Impact Assessment* (Halcrow MWT, 2009), contained in the overarching Environmental Impact Statement (EIS) document.

## 1.2 Purpose of this Report

The purpose of this report is to further enhance the findings of the RIA, which was developed from a comprehensive set of SIDRA analyses. Although SIDRA is a robust and industry accepted software package, its intersection evaluation can be somewhat limited when more complex network considerations come into play. This could include situations where intersections are closely spaced or operating under signal co-ordination. Microsimulation packages can incorporate all of these network considerations, in addition to providing a visual medium in which to observe the modelled future scenarios. For the purposes of this project, microsimulation modelling was undertaken within the latest Paramics V6.5 software package.

A site investigation in 2008 of the broader Gladstone transport network revealed that there are two areas that would benefit from additional microsimulation modelling. These areas are:

- The section of Glenlyon Road which is bound by William Street in the north and Tank Street in the south; and
- The Dawson Highway/Phillip Street signalised roundabout.

These locations are shown in Figure 2-1.

### 1.3 Structure of this report

The microsimulation assessment is presented in this report in the following sections:

- **Section 2** describes the scope of the assessment.
- **Section 3** describes the model development process (methodology) and outlines the raw data that was utilised in order to create the models.
- **Section 4** presents the results of the network analysis; and
- **Section 5** presents the study conclusions.

## 2 Scope of Assessment

### 2.1 Study Area

The scope of the assessment was separated into two model areas. These areas are indicated in Figure 2-1.

Model 1 encompasses the following intersections:

- Glenlyon Road /William Street;
- Glenlyon Road /Port Access Road/Railway Street;
- Glenlyon Road /Bramston Street/Dawson Highway;
- Glenlyon Road /Herbert Street;
- Glenlyon Road /Tank Street; and
- Bramston Road /Goondoon Street.

The Model 1 area was selected as it encompasses the key confluence of the two major roads within Gladstone City and will therefore form part of the likely route choice for peak construction generated traffic when Auckland Point is utilised. Site investigations also revealed that this area has the greatest potential for impact due to the existing levels of congestion observed during the peaks. In addition to the above, the intersections within the modelled area are closely spaced (in the vicinity of Port Access Road) and signal co-ordination exists for the intersections located at Port Access Road and Bramston Street.

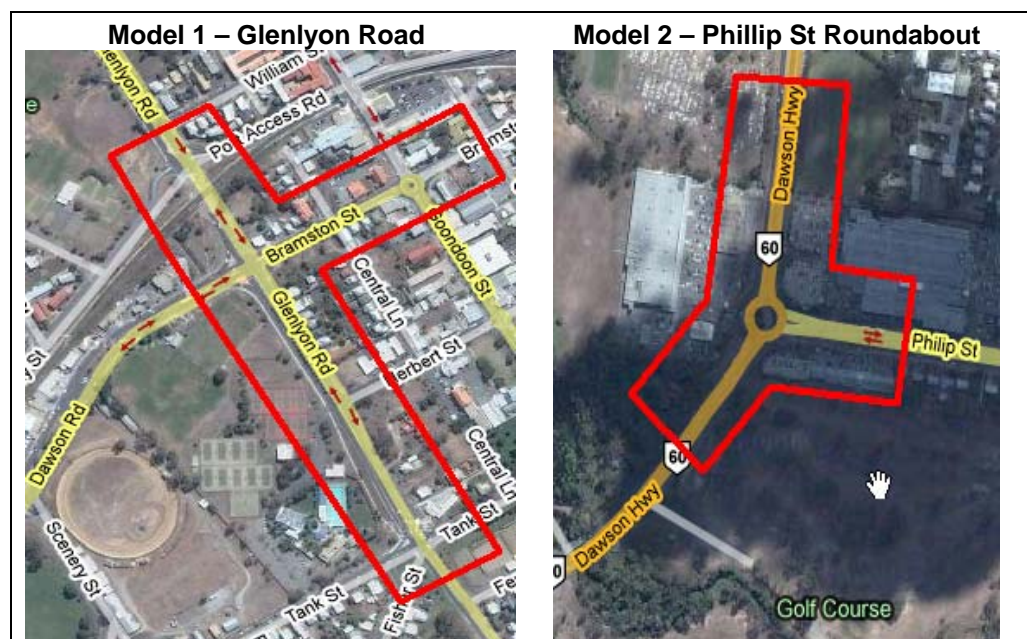


Figure 2-1 Study Area

Model 2 incorporates the area surrounding the Dawson Highway/Phillip Street roundabout. This region was selected not only because of the observed levels of congestion, but also due to the presence of signal metering on the roundabout. As mentioned in the RIA, SIDRA is able to roughly approximate intersection performance through a series of iterations involving analysis of performance ‘with’ and then ‘without’ the meter. Given the coarseness of this technique it was considered that microsimulation was a more appropriate tool for evaluating likely future year performance.

## 2.2 Scenarios for Assessment

The scenarios for assessment are summarised in Table 2-1. These scenarios represent a selection of the full assessment undertaken for the RIA. The selected scenarios represent the base reference scenario (i.e. Construction Camp Option D) along with a complete set of reference years without the proposed development. It should be noted that due to the adopted traffic assignment, there is no difference in modelled volumes at either model locations for road bridge option 1 and 2. Therefore, the assessment only includes the scenarios pertaining to road bridge option 1.

**Table 2-1 Traffic Assessment Scenarios**

Scenario / Year	No Dev	Construction			Operation			Road Option	Camp Option
		Train 1	Train 2	Train 3	Train 1	Train 2	Train 3		
Scenario 1 / 2008	✓							N/A	N/A
Scenario 2 / 2010	✓							N/A	N/A
Scenario 3d / 2010		✓	✓					N/A	D
Scenario 4 / 2013	✓							N/A	N/A
Scenario 5d / 2013			✓		✓			1	D
Scenario 7d / 2013			✓		✓			No Bridge	D
Scenario 12 / 2018	✓							N/A	N/A
Scenario 13d / 2018				✓	✓	✓		1	D
Scenario 15d / 2018				✓	✓	✓		No Bridge	D
Scenario 16 / 2021	✓							N/A	N/A
Scenario 17 / 2021					✓	✓	✓	1	N/A
Scenario 19 / 2021					✓	✓	✓	No Bridge	N/A

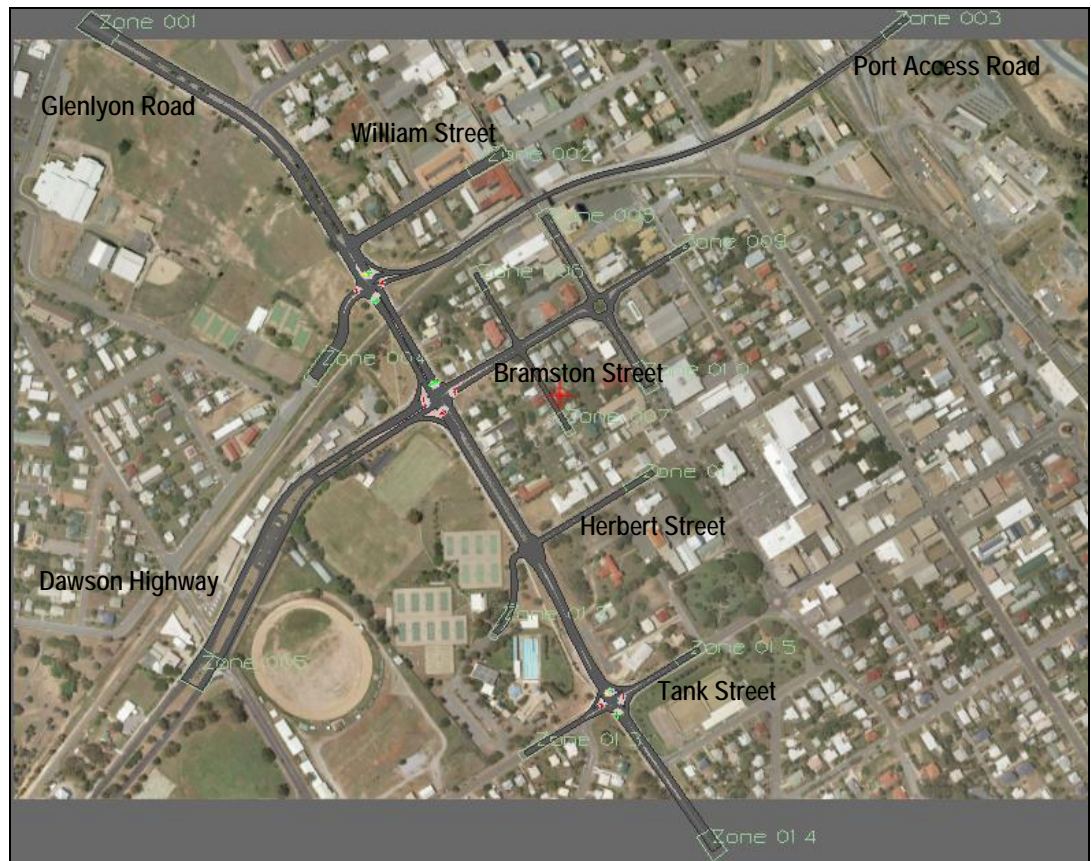


### 3 Model Development

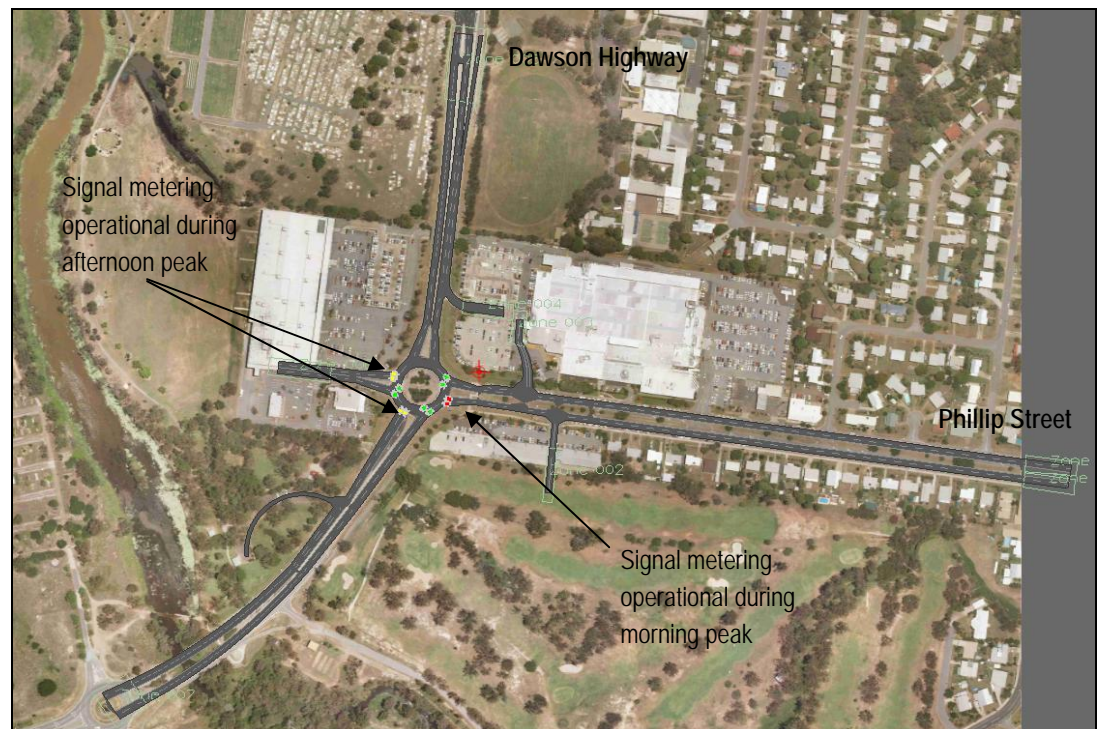
#### 3.1 Network Coding

The latest available aerial photograph was used at the time of model development to detail the microsimulation traffic models. This method allows for the precise replication of the existing road layout, including lane allocation, precise turn pocket lengths, turning lanes, and lane widths. The coded base case networks are shown in Figure 3-1 and Figure 3-2.

Traffic signal information throughout the base networks has been based on the use of fixed time signals and information obtained from DMR. Where signal coordination exists between intersections, details have been included within the model to replicate the existing conditions. A summary of DMR provided signal phasing data is included in Appendix A.



**Figure 3-1 Modelled Existing Network –Area 1 (Glenlyon Road)**



**Figure 3-2 Modelled Existing Network – Area 2 (Phillip Street Roundabout)**

## 3.2 Base Assumptions

Default Paramics model parameters have been used in the majority of the modelling process. These are validated and calibrated to replicate typical traffic conditions and have been used successfully in a vast number of simulation projects. Specific parameters have been changed in line with Halcrow-MWT standard practice and these include vehicle composition and the generalised cost coefficients. The value changes are based on fully adopted values by the New South Wales RTA and general peer acceptance of these values as best practice in replicating general Australian conditions.

## 3.3 Base Demand Matrix Estimation

### 3.3.1 Estimation Process

In order to replicate the existing traffic conditions for both the morning and evening peak hour periods, a 'matrix estimation' process was undertaken. This considers the relationship between link and turn flows and the desire to travel between origin and destination zones. The result is a matrix of trips that best replicates the observed trip patterns and is validated against known traffic count information.

Analysis of classified turning count data revealed that varying trip patterns emerge for different vehicle classifications. In order to accurately model current travel behaviour, 4 separate matrices were developed for the base models. These matrices are detailed as follows:

- Matrix 1 – Light vehicles – includes AUSTRROADS class 1 and 2;
- Matrix 2 – Heavy rigid vehicles – includes AUSTRROADS class 3, 4 and 5;
- Matrix 3 – Heavy vehicles – includes AUSTRROADS class 6, 7, 8 and 9; and
- Matrix 4 – Oversize heavy vehicles – includes AUSTRROADS class 10 and 11.

### 3.3.2 Base Traffic Generating Assumptions

The findings presented in this report are based upon the traffic generating assumptions and methodology discussed within the RIA. Since undertaking the microsimulation modelling exercise elements of the traffic generation have been revised, a summary of these changes is provided in Table 3-1 below.

**Table 3-1 RIA Original and Refined Assumptions**

Original Assumptions <sup>1</sup>	Refined Assumptions <sup>2</sup>
1. 2000 personnel for the Train 1 and 2 construction phase;	1. 1500 personnel for the Train 1 and 2 construction phase;
2. Fortnightly rotation assumption of 10 days on/4 days off;	2. 9 days on a fortnight (i.e. 5 days on/2 days off, then 4 days on/3 days off, being 90 hours per fortnight);
3. Hybrid Construction Camp Option D all non local personnel residing in the camp (i.e. 45% of total workforce);	3. Hybrid Construction Camp Option D all non local personnel residing in the camp (i.e. 30% of total workforce);
4. Anticipated pipeline movements are: <ul style="list-style-type: none"> <li>• Dawson Highway – 168 trucks/day for 167 days; and</li> <li>• Gladstone Mt Larcom Road – 54 trucks/day for 21 days; and</li> </ul>	4. Gladstone Port for the receipt of 260kms of 42" pipe in 18m lengths, 3 lengths/truck – equates to on average 20 trucks/day. On average 1.08 km/day of pipe moved over 25 day duration, equating to 10-11 month pipe transportation. Transport of 25km of pipe/ship/month, total 11 ships on average by end 2011.
5. Operations Phase Train 1 and 2 – 104 personnel, and Train 3 130 personnel.	5. Operations Phase Train 1 and 2 – 76 personnel, and Train 3 – 100 personnel.

<sup>1</sup> Used within RIA and microsimulation model

<sup>2</sup> Not used in RIA or microsimulation but covered by the original assumptions

The refined assumptions are important considerations when reviewing the microsimulation results. The results included within this report represent a ‘worst case scenario’ and demonstrate that there is significant ‘headroom’ factored into the microsimulation, exemplified by the following:

- Anticipated peak employee requirements are to be reduced by 25%, from 2000 personnel to 1500 personnel;
- Employee movements will be distributed over 4 movements in a fortnight rather than the 2 movements currently assumed within this report;
- Anticipated daily truck movements will also decrease; and

- Operations personnel will be slightly reduced from the 104 assumed within this report to 76 for Train 1 and 2. A slight reduction is also anticipated for Train 3 operations, with 130 personnel being reduced to 100 personnel.

The proposed mitigation measures presented in this report are based upon the ‘worst case scenario’ and are not reflective of the refined assumptions mentioned in Table 3-1 above.

### 3.3.3 Validation Process

The developed base matrices are assigned to the modelled road network after which link and turn data is extracted and compared to the base count data set to ensure that the two data groups match (within an acceptable GEH range).

Once the assignment estimation loop is completed and the vehicle flows are accepted the overall model is deemed to be validated and ‘fit for purpose’.

In order to assess the relationship between the assigned flows and the observed data set, the GEH statistic has been used. The GEH statistic is commonly used in modelling to evaluate the accuracy of modelled volumes when compared to actual flows. The standard protocol used for modelling validation is to endeavour to establish GEH values below 10, with any value between 5 and 10 representing a good match while GEH values less than 5 are considered to be very good matches and values over 10 should be investigated and where necessary either explained or rectified.

The model validation tables in Appendix B demonstrate that the base micro-simulation models for the project are considered to be suitably accurate representations of actual flows within the 2 model cordons. All turn movements have an acceptable GEH factor of less than 5 during both morning and afternoon peak periods.

GEH is a statistical analysis method developed by Geoffrey E. Havers in the 1970’s in the United Kingdom and is a form of Chi-squared statistic. It is now adopted as a key measure of network validation throughout the traffic modelling industry.

The formula for the GEH statistic is:  $GEH = \sqrt{(M-C)^2 / (0.5 \times (M+C))}$   
*where M = modelled flows and C = observed values*

## 3.4 Future Demand Matrix Estimation

### 3.4.1 Background Traffic

In line with the historical data analysis undertaken for the RIA, an annual growth of 5% and 3% (compounding) has been adopted for rural and urban roads, respectively.

### 3.4.2 Development Traffic

Separate matrix files were developed for all future years with the development. Development generated traffic was determined through the traffic generation and assignment process detailed within the RIA. Development related matrices are detailed as follows:

- Matrix 5 – Development Traffic Light Vehicles – includes AUSTROADS class 1 and 2;
- Matrix 6 – Development Traffic Heavy Vehicles – includes AUSTROADS class 3 and 9; and
- Matrix 7 – Development Traffic Bus – equivalent to AUSTROADS class 3.

## 4 Network Analysis

### 4.1 Existing Network Configuration

The 'do nothing' network (i.e. the existing network configuration, see Figure 3-1 and Figure 3-2) was tested with the future demand matrices, 'with' and 'without' the proposed LNG facility. Results are presented in Sections 4.1.1 and 4.1.2 below.

#### 4.1.1 Model 1 – Glenlyon Road

A summary of SIDRA and Paramics findings for Model 1 at Glenlyon Road are presented in Table 4-1. The SIDRA findings are taken from the results provided in the *Queensland Curtis LNG Project EIS Traffic and Transport Impact Assessment* (Halcrow MWT, 2009) whilst the Paramics findings are a summary of visual inspection, coupled with analysis of the extracted network operational characteristics (results provided in Table 4-2).

**Table 4-1 Model 1 Network Performance – Commentary 'Do Nothing'**

	SIDRA*	Paramics
Scenario 1	Individual intersections are either at or close to saturation. The only intersection operating with acceptable DOS is Port Access Road.	Visually, the network operates adequately. No improvements are required.
Scenario 2		
Scenario 3d	All intersections are operating at or above saturation.	Paramics confirms that the network requires remedial works. Visual inspection indicates that the cause of degradation originates from the heavy demand into and out of Port Access Road from Glenlyon Road.
Scenario 4	Individual intersections are either at or close to saturation. The only intersection operating with acceptable DOS is Port Access Road.	The network operates adequately in the morning peak, however, slight adjustments to the signal phasing is required in the afternoon peak. Additional green time allocation for the southbound movement will improve operations to acceptable levels.
Scenario 5d	All intersections are operating at or above saturation.	Paramics confirms that the network requires remedial works. In the morning peak the source of the congestion originates from the Dawson Highway/Glenlyon Road and Port Access Road intersections, with heavy northbound movements being unable to clear the intersections within the allocated green time. As would be expected, the reverse occurs in the afternoon peak.
Scenario 7d	All intersections are operating at or	During the morning peak, the network

	above saturation.	
Scenario 12	Not tested within SIDRA.	performs adequately for Scenarios 7d, 12, 13d and 15d. However, signal reconfiguration is required in the afternoon peak to accommodate the oversaturated southbound movements under a 'do nothing' network.
Scenario 13d		
Scenario 15d		
Scenario 16		During morning peak operations, a small amount of vehicle blocking is observed at the Tank Street intersection. Reconfiguration of signal timing will rectify the issue. For the afternoon peak, the issues identified in the previous Scenarios (i.e. 7d to 15d) are also observed for Scenarios 16, 17 and 19. Therefore, similar to the above, additional green time allocation is required for the southbound movement from Glenlyon Road (north).
Scenario 17		
Scenario 19		

\* Information pertains to Glenlyon Road intersecting at Port Access Road, Dawson Highway and Tank Street  
 Information extracted from *Queensland Curtis LNG Project EIS Traffic and Transport Impact Assessment* (Halcrow MWT, 2009)

The data presented in Table 4-2 was extracted from Paramics and colour coded according to the severity of performance degradation. The severity has been judged through consideration of the number of blocked vehicles, the decrease in average vehicle speed and general engineering judgement obtained from visual inspection of the models.

The number of blocked vehicles represents the number of vehicles which are queued outside of the model boundary at the end of the simulated period. This is effectively an indication of the latent demand and increased numbers of blocked vehicles indicate undesirable operations. However, the presence of blocked vehicles does not automatically indicate poor network performance. In cases where signalised intersections are located close to the model cordon, the reported number of blocked vehicles could simply be the usual queuing during a red phase. Upon return to green, all vehicles would then be released and the number of blocked vehicles would then return to zero. Another situation where the presence of blocked vehicles would be deemed to be acceptable is when there is adequate space for vehicles to queue, and the presence of the queue would not impact upon the operations of the rest of the network. An example of this is Port Access Road, where the adjacent intersection at Tug Berth Access Road is located more than 800m from Glenlyon Road.

The vehicle kilometres travelled (VKT) is the summation of all kilometres travelled for all vehicles which have passed through the network during the simulated period. A decrease in the VKT indicates that a smaller proportion of trips have been able to be completed during the simulation period. The vehicle hours travelled (VHT) is the summation of travel time for all vehicles which have passed through the network during the simulation period. Increases in VHT represent greater delays.

The five items that have been reported upon are intermingled and a decrease in performance in one criterion is matched with a decrease in performance in all other criteria also. For example, a substantial increase in the number of blocked vehicles indicates that congestion levels have increased, which therefore leads to decreased travel speeds and VKT and increased VHT.

Based on the results reported in Table 4-2, an alternative network configuration has been detailed for Scenario 3d (see Section 4.2.1). The revised network was then tested against all other future demands which did not perform adequately under the 'do nothing' network configuration (i.e. Scenarios 5d through to 19). No further modelling is required for Scenarios 1, 2 or 4.



**Table 4-2 Model 1 Network Performance – Model Results (Existing Network)**

	Scenario											
	1	2	3d	4	5d	7d	12	13d	15d	16	17	19
<b>AM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>	39	37	6	36	6	31	26	23	24	19	23	19
VKT <sup>2</sup>	2640	2775	2305	3035	2305	3435	3475	3775	3650	3710	3830	3680
VHT <sup>3</sup>	70	80	375	85	375	135	135	175	165	205	165	210
No. blocked vehicles <sup>4</sup>	0	0	1720	0	1720	30	30	40	20	80	80	110
% veh blocked <sup>5</sup>	0.00%	0.00%	39.03%	0.00%	44.75%	0.76%	0.76%	0.96%	0.49%	1.86%	1.85%	2.55%
<b>PM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>	15	14	6	10	5	4	5	5	4	5	4	5
VKT <sup>2</sup>	2615	2615	2630	2980	2580	2310	2630	2630	2480	2570	2475	2630
VHT <sup>3</sup>	250	250	440	300	515	535	575	575	570	585	560	545
No. blocked vehicles <sup>4</sup>	0	50	1470	160	960	1000	1330	1170	1290	1320	1450	1280
% veh blocked <sup>5</sup>	0.00%	1.46%	31.16%	4.28%	22.90%	25.03%	30.75%	25.60%	28.89%	27.98%	30.50%	27.03%

<sup>1</sup> The average vehicle speed is taken as the mean speed for all vehicles within the simulated period and includes geometric delays and stopped time at intersections

<sup>2</sup> VKT = Vehicle Kilometres Travelled

<sup>3</sup> VHT = Vehicle Hours Travelled

<sup>4</sup> The number of blocked vehicles represents the number of vehicles which are queued outside of the model cordon at the end of the simulated period

<sup>5</sup> Represents the number of blocked vehicles as a proportion of the matrix total

**Legend**

	Network performs adequately, no further modelling required
	Minor adjustments are required in order to improve operations to acceptable
	Serious network deficiencies, further investigation required

#### 4.1.2

### Model 2 – Dawson Highway/Phillip Street Roundabout

Similar to the process detailed for Model 1, a summary of SIDRA and Paramics findings for Model 2 at the Dawson Highway/Phillip Street roundabout are presented in Table 4-3. The SIDRA findings are taken from the results provided in the *Queensland Curtis LNG Project EIS Traffic and Transport Impact Assessment* (Halcrow MWT, 2009) whilst the Paramics findings are a summary of visual inspection, coupled with analysis of the extracted network operational characteristics (results provided in Table 4-4).

**Table 4-3 Model 2 Network Performance – Commentary ‘Do Nothing’**

	SIDRA*	Paramics
Scenario 1	Unsignalised roundabout arrangement identified serious operational deficiencies for all future and base year conditions (excluding the 2008 AM Peak).	Visually, the network operates adequately. No improvements are required.
Scenario 2		
Scenario 3d		During morning peak operations, the southern Dawson Highway and eastern Phillip Street approaches are oversaturated. For the afternoon peak, the heavy southbound demand from the northern Dawson Highway approach restricts vehicles from entering the roundabout at Phillip Street. In the afternoon, the northern Dawson Highway and eastern Phillip Street approaches are oversaturated.
Scenario 4		The blocked vehicles during the morning peak originate from the Phillip Street approach. Signal reconfiguration is likely to improve operations back to acceptable.
Scenario 5d		Similar problems to those identified for Scenario 3d are inherent to Scenarios 7d through to Scenario 19. During the morning peak the southern Dawson Highway and eastern Phillip Street approaches are oversaturated, whilst in the afternoon, the northern Dawson Highway, eastern Phillip Street and western shopping centre approaches are oversaturated. Operations get progressively worse with each future year.
Scenario 7d		
Scenario 12		
Scenario 13d		
Scenario 15d		
Scenario 16		
Scenario 17		
Scenario 19		

\* Information extracted from *Queensland Curtis LNG Project EIS Traffic and Transport Impact Assessment* (Halcrow MWT, 2009)

Similar to the process discussed above in Section 4.1.1, the data presented in Table 4-4 was extracted from Paramics and colour coded according to the severity of performance degradation. The severity has been judged through consideration of the number of blocked vehicles, the decrease in average vehicle speed and general engineering judgement obtained from visual inspection of the models.

Based on the results reported in Table 4-4, an alternative network configuration has been detailed for Scenario 3d (see Section 4.2.2). The revised network was then tested against all other future demands which did not perform adequately under the ‘do

nothing' network configuration (i.e. Scenarios 5d through to 19). No further modelling is required for Scenarios 1, 2 or 4.

**Table 4-4 Model 2 Network Performance – Model Results (Existing Network)**

	Scenario											
	1	2	3d	4	5d	7d	12	13d	15d	16	17	19
<b>AM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>	43	24	13	18	15	10	12	11	9	9	9	9
VKT <sup>2</sup>	2830	2935	3195	3095	3160	3200	3335	3345	3335	3430	3415	3440
VHT <sup>3</sup>	65	125	250	180	210	335	285	315	380	370	380	380
No. blocked vehicles <sup>4</sup>	0	10	170	80	160	550	320	390	680	630	650	660
% veh blocked <sup>5</sup>	0.00%	0.29%	4.16%	2.09%	4.00%	12.19%	7.21%	8.61%	14.15%	12.99%	13.36%	13.48%
<b>PM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>	48	44	11	26	18	11	11	10	9	9	7	9
VKT <sup>2</sup>	3320	3490	3445	3725	3745	3785	3830	3865	3860	3970	3170	3985
VHT <sup>3</sup>	70	79	315	150	210	360	345	375	3970	465	370	465
No. blocked vehicles <sup>4</sup>	0	0	380	30	70	650	470	550	880	810	660	850
% veh blocked <sup>5</sup>	0.00%	0.00%	7.80%	0.63%	1.43%	11.90%	8.54%	9.83%	14.90%	13.48%	10.95%	14.04%

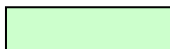
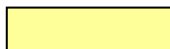

<sup>1</sup> The average vehicle speed is taken as the mean speed for all vehicles within the simulated period and includes geometric delays and stopped time at intersections

<sup>2</sup> VKT = Vehicle Kilometres Travelled

<sup>3</sup> VHT = Vehicle Hours Travelled

<sup>4</sup> The number of blocked vehicles represents the number of vehicles which are queued outside of the model cordon at the end of the simulated period

<sup>5</sup> Represents the number of blocked vehicles as a proportion of the matrix total

Legend	
	Network performs adequately, no further modelling required
	Minor adjustments are required in order to improve operations to acceptable
	Serious network deficiencies, further investigation required

## 4.2 Future Network Configuration

Based on the outcomes of the 'do nothing' analyses a number of scenarios have been flagged as requiring remedial works. The 'do something' solutions, along with the model results, are presented in Sections 4.2.1 and 4.2.2 below.

### 4.2.1 Model 1 – Glenlyon Road

The 'do nothing' results presented in Section 4.1.1 indicated that upgrade works will be required for 2010 'with development' conditions (i.e. Scenario 3d). Extensive model testing has concluded that to accommodate the anticipated 2010 'with development' volumes, the following works will be required:

#### *Glenlyon Road/Port Access Road Intersection*

- To accommodate the heavy afternoon peak, development generated traffic demand from Port Access Road into the Dawson Highway, a dual left turn signalised slip lane is required on the Port Access Road approach (shown in Figure 4-1); and
- Similar to existing, signal coordination needs to be retained between the Port Access Road intersection and the Dawson Highway intersection. However, the signal cycle time also needs to be extended to 150 seconds.

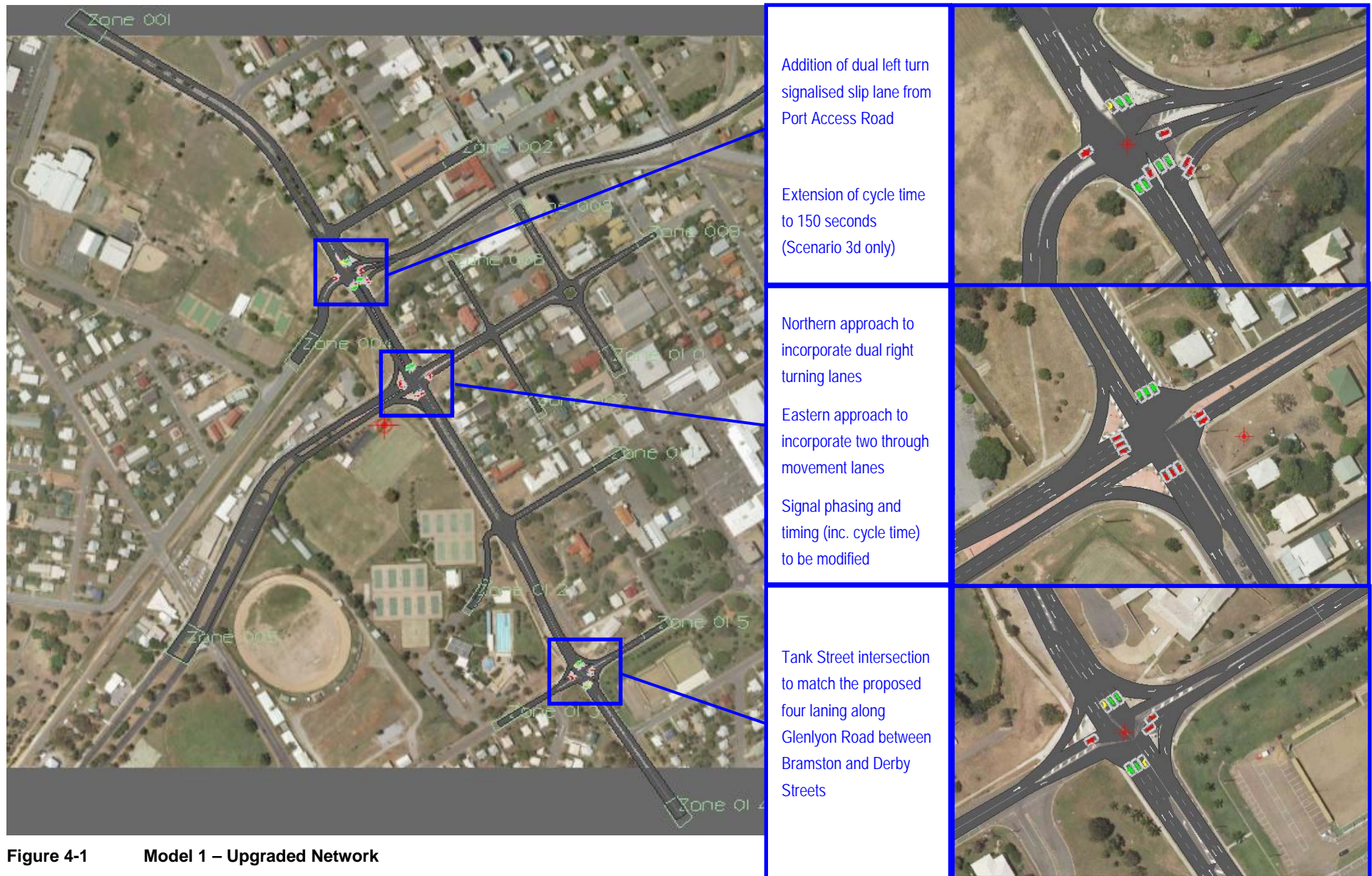
#### *Glenlyon Road/Dawson Highway/Bramston Street Intersection*

- To allow for coordination between this intersection and Port Access Road, the signal cycle time requires to be extended to 150 seconds;
- The northern approach should be reconfigured to cater for a dual right turn lane (middle lane to be shared through/right) and the turn pocket should be extended as far north as practicable (bearing in mind the constraints of the rail bridge);
- The eastern approach is to remain as two approach lanes. However, the lane designation for the median lane should accommodate a shared right/through movement. This means that the eastern approach will allow for through movements on both approach lanes; and
- Following the reconfiguration of lane designation on the northern and eastern approaches, modifications to the signal phasing arrangements are required.

#### *Glenlyon Road/Tank Street Intersection*

- The microsimulation modelling confirms that the already proposed four laning of Glenlyon Road between Bramston and Derby Streets is required. No other modifications are required.

Note that there are some discrepancies between the RIA and microsimulation findings. Where discrepancies exist, the findings of the microsimulation supersede that of the RIA.



**Figure 4-1 Model 1 – Upgraded Network**

The results for the upgraded network (Model 1) are provided in Table 4-5 below. As can be seen in the results, the proposed network operates satisfactorily for all future years, 'with' and 'without' the proposed development.

It should be noted that the traffic distribution changes after 2010 (Scenario 3d). This is due to the presence of the road bridge, or the shifting of water transport access to the end of Alf O'Rourke Drive rather than Auckland Point. Model testing has shown that the revised traffic volumes (post 2010) are able to be accommodated within the layout presented above with some minor signal phasing changes. In addition to this, a cycle time of 150 seconds is no longer required and the Dawson Highway and Port Access Road intersections are able to operate satisfactorily with a cycle time ranging from 100 – 120 seconds.

**Table 4-5 Model 1 Network Performance – Model Results (Upgraded Network)**

	Scenario											
	1	2	3d	4	5d	7d	12	13d	15d	16	17	19
<b>AM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>			18		37	37	33	32	33	30	32	31
VKT <sup>2</sup>			4660		3735	3490	3600	3935	3805	3630	3705	3870
VHT <sup>3</sup>			260		100	95	110	120	115	120	115	125
No. blocked vehicles <sup>4</sup>			0		0	0	0	0	0	0	0	0
% veh blocked <sup>5</sup>			0.00%		0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
<b>PM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>			17		32	36	35	31	34	33	32	32
VKT <sup>2</sup>			5025		4300	3995	4115	4520	4390	4585	4600	4590
VHT <sup>3</sup>			300		135	110	115	145	130	140	140	140
No. blocked vehicles <sup>4</sup>			150		0	0	0	0	0	0	0	0
% veh blocked <sup>5</sup>			4.66%		0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%

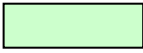
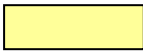


<sup>1</sup> The average vehicle speed is taken as the mean speed for all vehicles within the simulated period and includes geometric delays and stopped time at intersections

<sup>2</sup> VKT = Vehicle Kilometres Travelled

<sup>3</sup> VHT = Vehicle Hours Travelled

<sup>4</sup> The number of blocked vehicles represents the number of vehicles which are queued outside of the model cordon at the end of the simulated period

<sup>5</sup> Represents the number of blocked vehicles as a proportion of the matrix total

Legend	
	Network performs adequately, no further modelling required
	Given the constraints of the site, operation is acceptable
	Serious network deficiencies, further investigation required
	Assessment has not been undertaken



4.2.2

**Model 2 – Dawson Highway/Phillip Street Roundabout**

The ‘do nothing’ results presented in Section 4.1.2 indicated that upgrade works will be required for 2010 ‘with development’ conditions (i.e. Scenario 3d). Based on the existing geometric constraints of the site, only one improvement may be accommodated, and this involves the inclusion of a left turn slip lane from Phillip Street into Dawson Highway (south), as shown in Figure 4-2. The modelled configuration has been cross-checked against the requirements set out in the *Road Planning and Design Manual – Part 14 Roundabouts* (DMR, 2006) and preliminary investigations indicate that the slip lane can be accommodated. However, the exact geometry and hence, suitability will need to be drawn and detailed by a qualified road designer using appropriate software tools such as AutoCAD.



**Figure 4-2 Model 2 – Upgraded Roundabout**

The results (see Table 4-6) indicate that the upgraded roundabout is able to provide acceptable performance for Scenario 3d, 4 and 5d. However, if Scenario 7d proceeds further upgrade to signalisation will be required by 2013. Otherwise, the upgrade to signalisation will be required at 2018, regardless of whether the development proposal proceeds.

**Table 4-6 Model 2 Network Performance – Model Results (Upgraded Roundabout)**

	Scenario											
	1	2	3d	4	5d	7d	12	13d	15d	16	17	19
<b>AM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>			15	29	17	10	14					
VKT <sup>2</sup>			3245	3225	3215	3220	3445					
VHT <sup>3</sup>			220	115	195	335	255					
No. blocked vehicles <sup>4</sup>			130	10	110	520	220					
% veh blocked <sup>5</sup>			3.18%	0.26%	2.75	11.52%	4.96%					
<b>PM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>			29	30	31	13	17					
VKT <sup>2</sup>			3885	3770	3930	4010	4155					
VHT <sup>3</sup>			135	125	125	310	245					
No. blocked vehicles <sup>4</sup>			30	10	10	420	200					
% veh blocked <sup>5</sup>			0.62%	0.21%	0.20%	7.69%	3.64%					


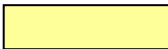


<sup>1</sup> The average vehicle speed is taken as the mean speed for all vehicles within the simulated period and includes geometric delays and stopped time at intersections

<sup>2</sup> VKT = Vehicle Kilometres Travelled

<sup>3</sup> VHT = Vehicle Hours Travelled

<sup>4</sup> The number of blocked vehicles represents the number of vehicles which are queued outside of the model cordon at the end of the simulated period

<sup>5</sup> Represents the number of blocked vehicles as a proportion of the matrix total

Legend	
	Network performs adequately, no further modelling required
	Given the constraints of the site, operation is acceptable
	Serious network deficiencies, further investigation required
	Assessment has not been undertaken

The upgraded signalised arrangement is indicated in Figure 4-3.



**Figure 4-3 Model 2 – Upgrade to Signalisation**

The proposed configuration includes the following:

*Northern Approach*

- Three stand up lanes and a short left turn slip lane. The stand up lanes are to consist of two dedicated through lanes and a dedicated right turn lane; and
- Three exit lanes, which is an increase from the existing of two. The kerbside lane is proposed to be a short downstream lane of approximately 100m.

*Eastern Approach*

- The left turn slip lane required as a result of Scenario 3d is retained as part of the signalised configuration; and
- Similar to existing, Phillip Street will remain as two stand up approach and exit lanes. However, the approach is to accommodate a dual right turn lane, with the kerbside stand up to incorporate a shared through and right turn movement.

*Southern Approach*

- Due to the anticipated heavy northbound movement in the future year morning peaks, the southern approach requires four approach lanes consisting of three through lanes (kerbside lane to be a shared left and through) and one short right turn lane; and
- The intersection located directly to the south also requires some minor adjustments so that the transition from the two lanes on Dawson Highway to the four lane flare is more gradual. Instead of the dedicated left turn auxiliary lane which is currently provided for the park access, it is proposed that this become a shared left and through lane as indicated in Figure 4-3 above.

*Western Approach*

- The proposed configuration on the western approach will match the existing provision of two approach and two exit lanes.

The results presented in Table 4-7 indicate that the signalised arrangement provides adequate capacity for all years, leading up to and including 2021 'with' the proposed development (i.e. Scenario 19).

**Table 4-7 Model 2 Network Performance – Model Results (Upgraded to Signalisation)**

	Scenario											
	1	2	3d	4	5d	7d	12	13d	15d	16	17	19
<b>AM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>						26	37	36	26	34	34	32
VKT <sup>2</sup>						3780	3740	3825	4025	4120	4125	4150
VHT <sup>3</sup>						150	100	105	160	120	125	130
No. blocked vehicles <sup>4</sup>						0	0	0	0	0	0	0
% veh blocked <sup>5</sup>						0.00%	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
<b>PM Peak</b>												
Ave veh speed (km/hr) <sup>1</sup>						25	27	23	19	20	19	18
VKT <sup>2</sup>						4240	4325	4370	4555	4680	4670	4645
VHT <sup>3</sup>						170	160	200	250	230	245	265
No. blocked vehicles <sup>4</sup>						10	20	30	80	20	40	100
% veh blocked <sup>5</sup>						0.18%	0.36%	0.54%	1.35%	0.33%	0.66%	1.65%

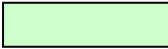
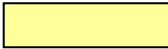


<sup>1</sup> The average vehicle speed is taken as the mean speed for all vehicles within the simulated period and includes geometric delays and stopped time at intersections

<sup>2</sup> VKT = Vehicle Kilometres Travelled

<sup>3</sup> VHT = Vehicle Hours Travelled

<sup>4</sup> The number of blocked vehicles represents the number of vehicles which are queued outside of the model cordon at the end of the simulated period

<sup>5</sup> Represents the number of blocked vehicles as a proportion of the matrix total

Legend	
	Network performs adequately, no further modelling required
	Given the constraints of the site, operation is acceptable
	Serious network deficiencies, further investigation required
	Assessment has not been undertaken

## 5 Conclusions

The microsimulation assessment for the proposed QCLNG project has been completed. A number of scenarios were assessed and these included the base reference scenario (i.e. Construction Camp Option D) along with a complete set of reference years without the proposed development.

The assessment was undertaken with due consideration of the findings of the RIA, *Queensland Curtis LNG Project EIS Traffic and Transport Impact Assessment* (Halcrow MWT, 2009) and has built upon the recommendations presented in that report. Based on the network analyses of the two modelled areas, a summary of remedial works are as follows:

### Works to be completed by 2010 – Scenario 3d

- Port Access Road to incorporate a dual left turn signalised slip lane, along with an extension of signal cycle time to 150 seconds;
- Dawson Highway/Glenlyon Road Intersection to incorporate minor lane reconfigurations on the northern and eastern approaches. Signal cycle time also to be extended to 150 seconds;
- Tank Street intersection to accommodate already proposed four laning of Glenlyon Road between Bramston and Derby Streets; and
- Phillip Street roundabout to incorporate a left turn slip lane from the Phillip Street approach into the Dawson Highway (south).

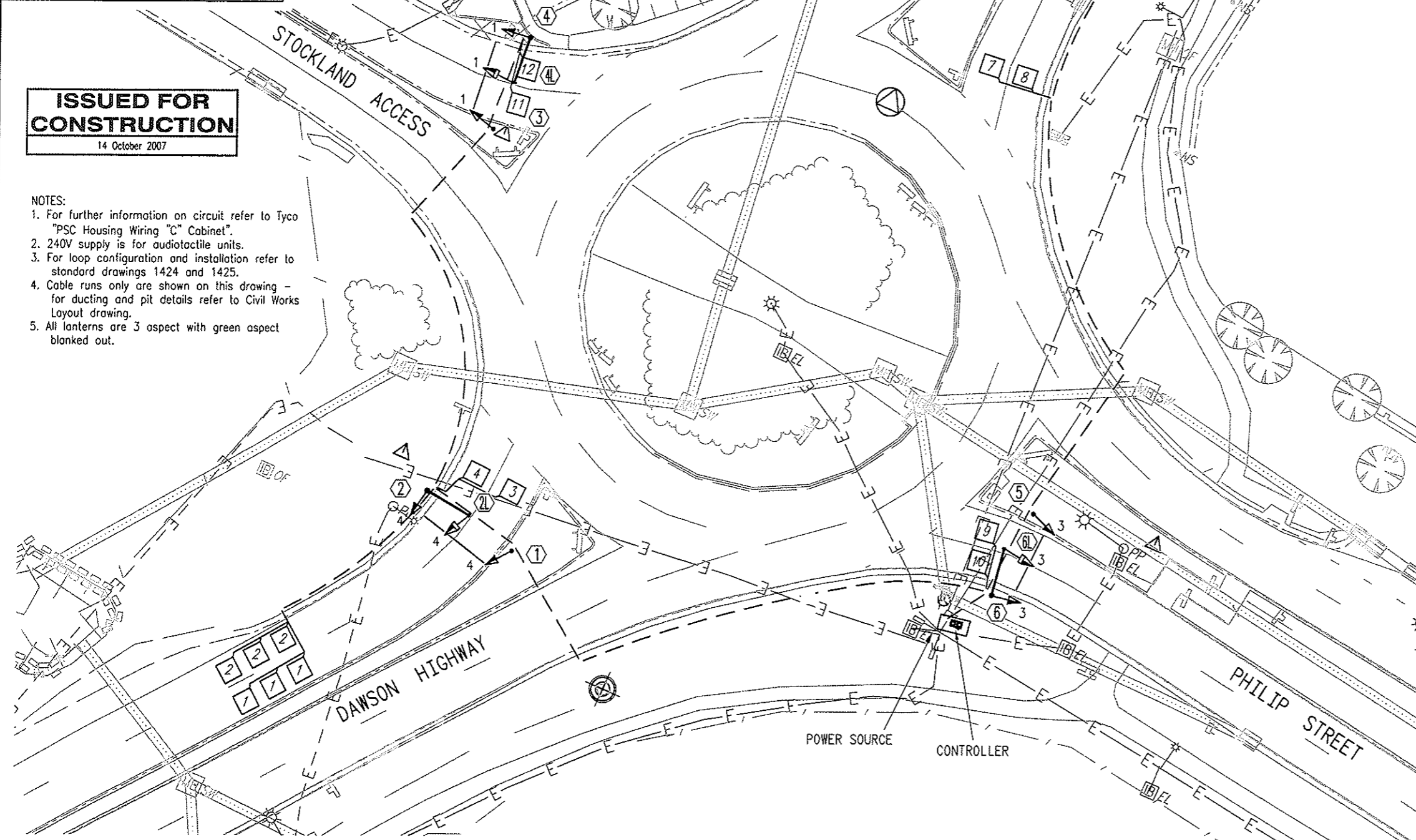
### Works required post 2010 – Scenario 5d – 19

- Cycle times and signal phasing to be optimised for Port Access Road, Dawson Highway/Glenlyon Road and Tank Street intersections to allow for the change in development generated traffic distribution;
- If the proposed road bridge between Curtis Island and Gladstone does not proceed, the roundabout at Dawson Highway/Phillip Street will need to be upgraded to full signalisation by 2013; and
- If the proposed road bridge between Curtis Island and Gladstone does proceed, the signalised roundabout is able to provide adequate service until 2018. Upgrade to full signalisation will be required in this year, even without the presence of the proposed development.

The results presented within this report and summarised above, represent a ‘worst case scenario’ and are not reflective of the refined assumptions discussed in Section 3.3.2.

# Appendix A. Base Coding – Signals & Int. Layout

Phase Diagrams			
Signal Groups		(3)	(1) (4)
Vehicle/Ped Groups		Vg3	Vg1 Vg4
Logical Input		1,2 3,4	5,6 7,8 5,6 7,8
Coil		Pres	Pres Pres
Extend		X	X X
Increment			
Special Conditions	A phase arterial in personality. SG2 to be programmed as Green (no lanterns). SG1, SG3 & SG4 to be programmed as Yellow, Red (no Green lantern)		



**ISSUED FOR CONSTRUCTION**  
14 October 2007

- NOTES:
- For further information on circuit refer to Tyco "PSC Housing Wiring "C" Cabinet".
  - 240V supply is for audiotactile units.
  - For loop configuration and installation refer to standard drawings 1424 and 1425.
  - Cable runs only are shown on this drawing - for ducting and pit details refer to Civil Works Layout drawing.
  - All lanterns are 3 aspect with green aspect blanked out.

Signal Groups	Function	Controller Terminals	Run 1 Connections				Run 2 Connections		Run 3 Connections		Run 4 Connections	
			Final Terminals	Cncts	Cncts	Cncts	Final Terminals	Cncts	Final Terminals	Cncts	Final Terminals	Cncts
1	Red	A5	1	1	1							
	Yellow	A4	2	2	2							
	Green	A3										
	Red	A8										
2	Yellow	A7										
	Green	A6										
3	Red	A11				5	5	5				
	Yellow	A10				6	6	6				
	Green	A9										
4	Red	A14	7	7	7							
	Yellow	A13	8	8	8							
	Green	A12										
5												
6												
7												
8												
9												
10												
11												
12												

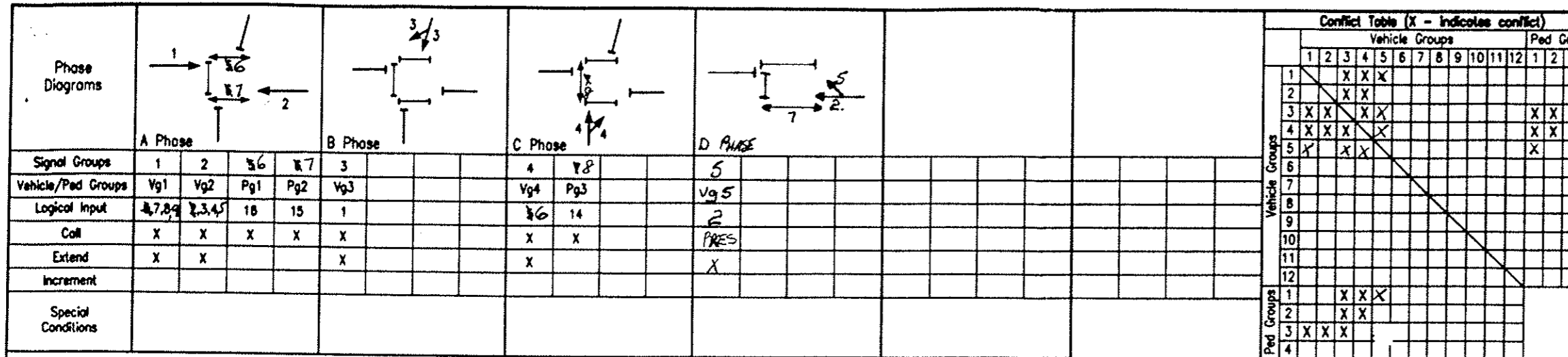
240V	A2	A	16	A	16
Det Common	E3	PR	Gy	PR	Gy
Neutral	A1, B1, C1, D1	N	Bk Bk Bk	N	Bk Bk
Spare Cores to earth link			3-6 9-15		1-4 7-15
Cable Size			19 19 19		19 19

Detector Table - PSC PD200 Series Integrated Detector System									
Physical Input	Controller Terminal	Logical Input	Loop/PB Configuration	Dist to Stop Line	Physical Input	Controller Terminal	Logical Input	Loop/PB Configuration	Dist to Stop Line
Loop 1	P1	1	Queue						17
Loop 2	P2	2	Queue						18
Loop 3	P3	3	Stop Line						19
Loop 4	P4	4	Stop Line						20
Loop 5	P5	5	Queue						21
Loop 6	P6	6	Queue						22
Loop 7	P7	7	Stop Line						23
Loop 8	P8	8	Stop Line						24
Loop 9	Q9	9	Counting						25
Loop 10	Q10	10	Counting						26
Loop 11	Q11	11	Counting						27
Loop 12	Q12	12	Counting						28
		13							29
		14							30
		15							31
		16							32

Filename: E:\Woods & Smith & Moore\Jobs in Progress\WIP\Gladstone\Gladstone & Caroline\4551\_378954.dwg Date: 06/07/2007 - 8:22 am  
 Xrefs: CAD FILES \\MR10150733\Signals.dwg; Layout: Electrical

Revisions	Certified	Date	Microfiled	Associated Job Nos	Survey Data	GLADSTONE CITY DAWSON HIGHWAY (GLADSTONE - BILOELA) DAWSON HWY & PHILIP ST				TRAFFIC SIGNAL INSTALLATION ITS DESIGN TYCO PSC-ID CONTROLLER				Site Number 4622	
					Horiz. Datum ISG 2000 Zone 56/1	Reference Points				Drawing R Smith	Design R Smith	Design Review 	Engineering Certification 	For scheme approval status refer Drg. No. 404050 (1 of 3)	Job No. 161/46A/205
					Azimuth Datum ISG 2000 Zone 56/1	Preceding RP 48A/2A				Checked J Chuong	Verified J Chuong	Date 10/07	RPEQ No. 2696	Contract No. 404052 A	Series Number 3 of 3
					Height Datum AHD derived	Dist. to start of job (km)				Through Chainage from Start of gazette					
					Survey Books MR85820-46A	From start to end of job				From end to Following RP					
A						0.00				4.78					

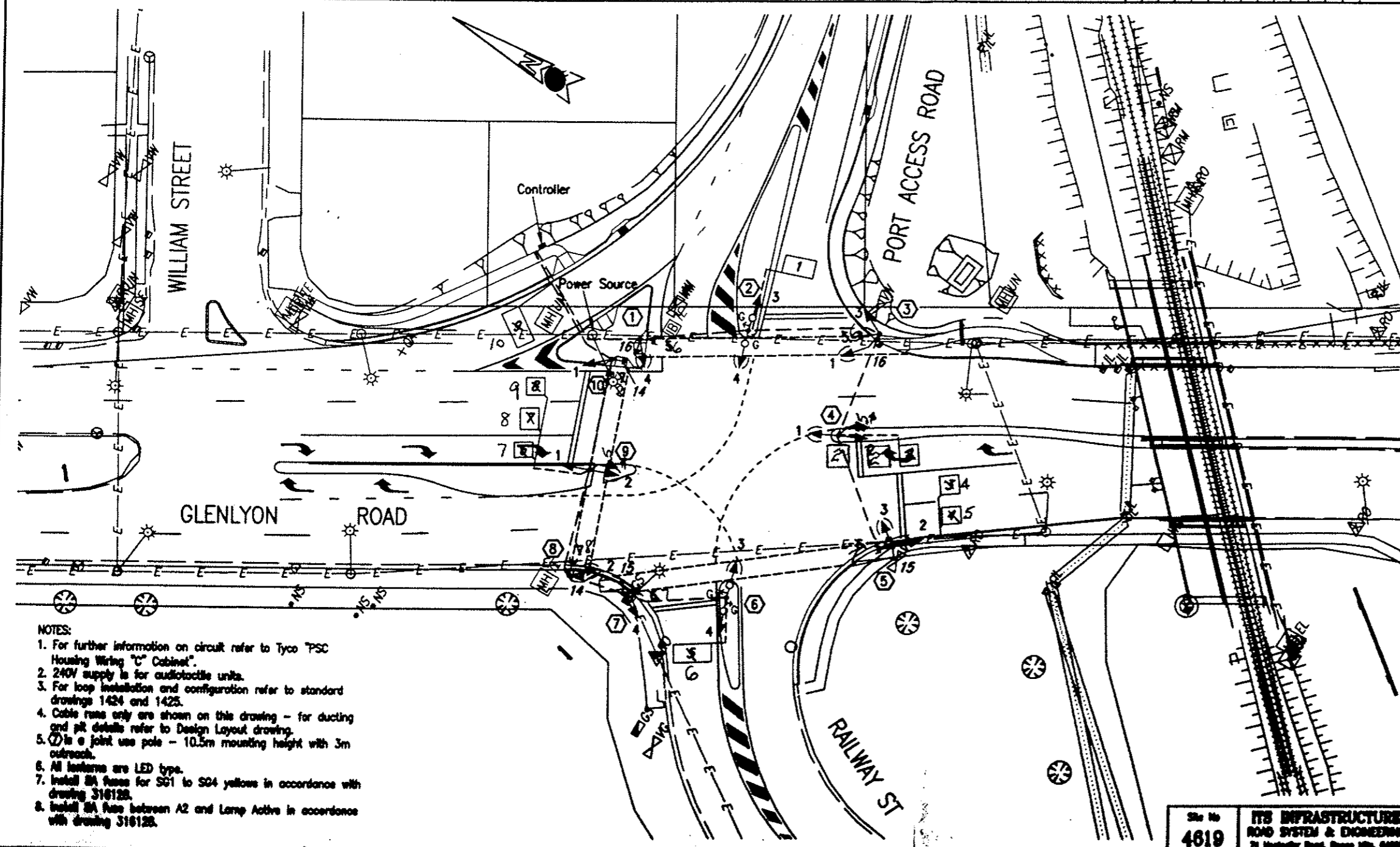




**Conflict Table (X - indicates conflict)**

Vehicle Groups	Vehicle Groups												Ped Groups			
	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4
1																
2																
3	X	X														
4	X	X	X													
5	X	X	X	X												
6																
7																
8																
9																
10																
11																
12																
1			X	X	X											
2			X	X												
3	X	X	X													
4	X	X	X	X												

Run	Connections		Connections		Connections		Connections	
	Final Terminals	Cores Used	Final Terminals	Cores Used	Final Terminals	Cores Used	Final Terminals	Cores Used
Run 1	1	1	1	1	1	1	1	1
Run 2	2	2	2	2	2	2	2	2
Run 3	3	3	3	3	3	3	3	3
Run 4	4	4	4	4	4	4	4	4
Run 5	5	5	5	5	5	5	5	5
Run 6	6	6	6	6	6	6	6	6
Run 7	7	7	7	7	7	7	7	7
Run 8	8	8	8	8	8	8	8	8
Run 9	9	9	9	9	9	9	9	9
Run 10	10	10	10	10	10	10	10	10
Run 11	11	11	11	11	11	11	11	11
Run 12	12	12	12	12	12	12	12	12
Run 13	13	13	13	13	13	13	13	13
Run 14	14	14	14	14	14	14	14	14
Run 15	15	15	15	15	15	15	15	15
Run 16	16	16	16	16	16	16	16	16
Run 17	17	17	17	17	17	17	17	17
Run 18	18	18	18	18	18	18	18	18
Run 19	19	19	19	19	19	19	19	19
Run 20	20	20	20	20	20	20	20	20
Run 21	21	21	21	21	21	21	21	21



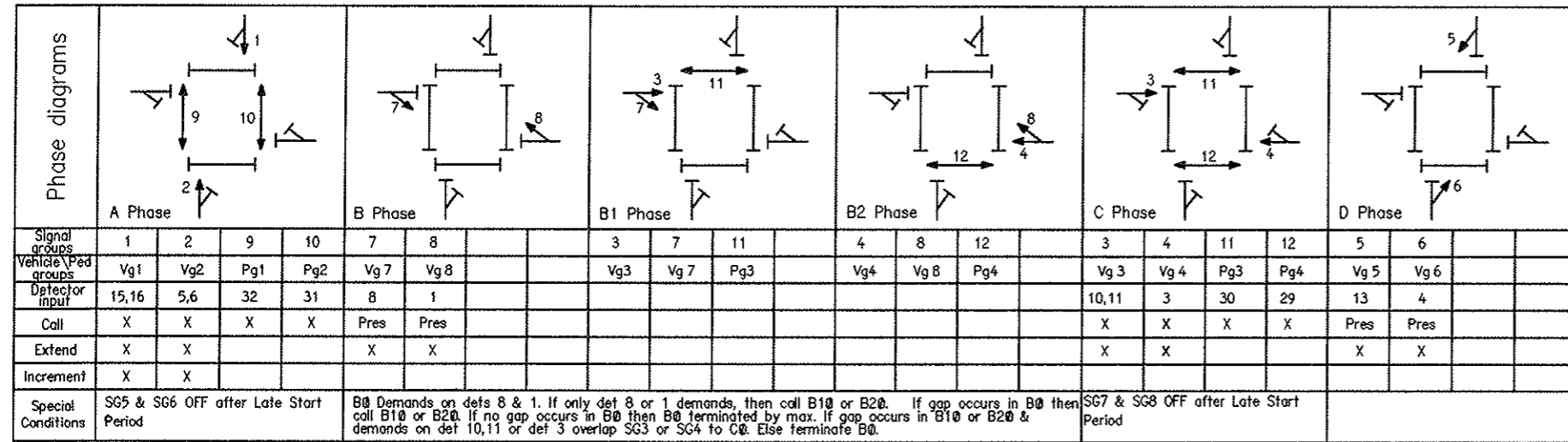
Run	Connections	Final Terminals	Cores Used
A2	240V (See Note 2)	32	0y
E5	Ext Det 1	22	22
E6	Ext Det 2	23	23
E7	Ext Det 3	24	24
E3	Det Common	26	26
A11	Neutral	NL	Blk
Spares Cores		13-17	22, 25
Cable Size		29	29

**Detector Table - PSC PD200 Series Integrated Detector System**

Physical Terminal	Controller Logical Input	Loop/PB Configuration	Detector Mode	Physical Terminal	Controller Logical Input	Loop/PB Configuration	Detector Mode
Loop 1	P1	1	Stop Line	17	17	17	Locked
Loop 2	P2	2	Stop Line	18	18	18	Locked
Loop 3	P3	3	Stop Line	19	19	19	Locked
Loop 4	P4	4	Stop Line	20	20	20	Locked
Loop 5	P5	5	Stop Line	21	21	21	Locked
Loop 6	P6	6	Stop Line	22	22	22	Locked
Loop 7	P7	7	Stop Line	23	23	23	Locked
Loop 8	P8	8	Stop Line	24	24	24	Locked
Loop 9	Q8	9	Counting	25	25	25	Locked
				26	26	26	
				27	27	27	
				28	28	28	
				29	29	29	
				30	30	30	
				31	31	31	
				32	32	32	

- NOTES:**
- For further information on circuit refer to Tyco PSC Housing Wiring "C" Cabinet.
  - 240V supply is for audiotactile units.
  - For loop installation and configuration refer to standard drawings 1424 and 1425.
  - Cable runs only are shown on this drawing - for ducting and pit details refer to Design Layout drawing.
  - ⊙ is a joint use pole - 10.5m mounting height with 3m outreach.
  - All lanterns are LED type.
  - Install 2A fuses for SG1 to SG4 yellows in accordance with drawing 316128.
  - Install 2A fuse between A2 and Lamp Active in accordance with drawing 316128.

<p><b>Revisions</b></p> <table border="1"> <tr><th>Revised</th><th>By</th><th>Date</th><th>Reason</th></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> </table>	Revised	By	Date	Reason					<p><b>Associated Job nos</b></p> <p>Dimensions in metres except where shown otherwise.                   Orvert size in millimetres.</p>	<p><b>Survey books</b></p> <p>NSR7977 to 7980-183                   NSR8029 to 8022-183</p>	<p><b>GLADSTONE CITY</b></p> <p><b>GLADSTONE PORT ACCESS ROAD</b></p> <p>CTL CHGE 00 - 858.257</p>	<p><b>ITS INFRASTRUCTURE ROAD SYSTEM &amp; ENGINEERING</b></p> <p>71 Mulgrave Road, Green Hills, QLD 4068</p>	<p><b>TRAFFIC SIGNAL INSTALLATION</b></p> <p><b>TYCO PSC-ID CONTROLLER</b></p> <p><b>CABLE CONNECTIONS</b></p>	<p><b>Queensland Government</b></p> <p>Department of Main Roads</p> <p><b>JOB No. 161/183/2</b></p> <p><b>Drawing No. 330167</b></p>
Revised	By	Date	Reason											
<p><b>How base dig &amp; notes changed</b></p> <p><b>Original base</b></p>	<p><b>Auxiliary drawing nos</b></p> <p>(Office use only)</p>	<p><b>Scales</b></p> <p>0 2 4 6 8 10m</p>	<p><b>Through chains from</b></p>	<p><b>Reference Points</b></p> <p>From start to end of job                   From end to following RPO</p>	<p><b>Approved</b></p> <p>T HM</p>	<p><b>Contract No. GEND/123</b></p> <p><b>7/4/03</b></p>								

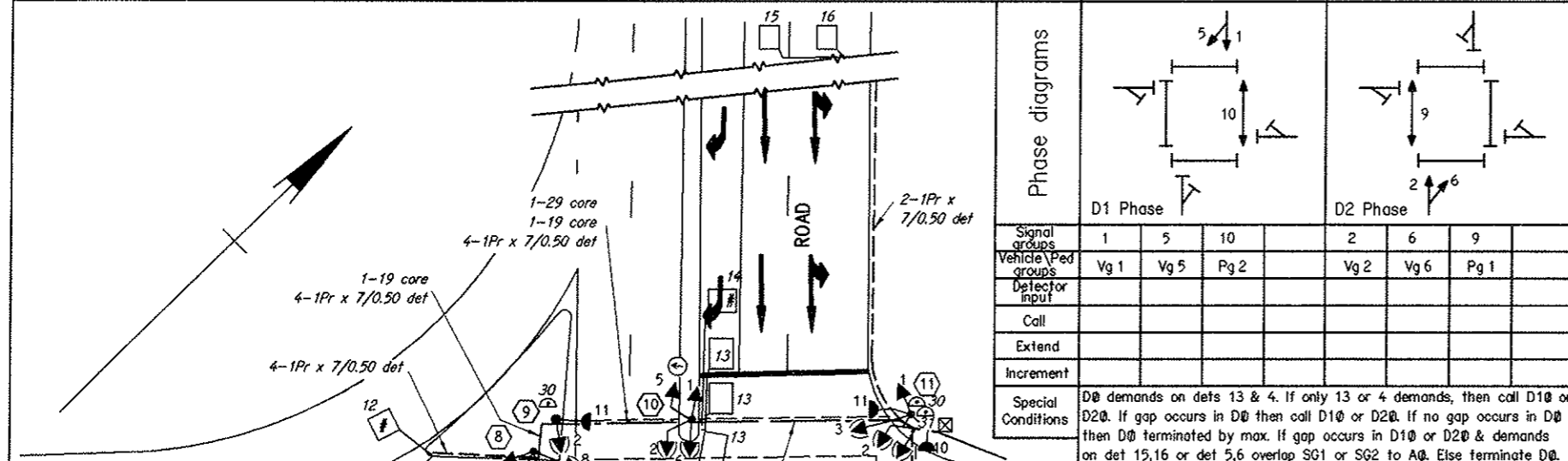


Conflict table (X - Indicates conflict)

Vehicle groups	Vehicle groups												Ped groups					
	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4		
1																		
2	X																	X
3	X	X												X	X		X	X
4	X	X	X											X	X		X	X
5	X	X	X	X										X	X		X	X
6	X	X	X	X	X									X	X		X	X
7	X	X	X	X	X	X								X	X		X	X
8	X	X	X	X	X	X	X							X	X		X	X
9																		
10																		
11																		
12																		

Controller terminals

Function	Run 1 connections	Run 2 connections	Run 3 connections	Run 4 connections
A5 Red 1	1	1	1	1
A4 Yellow 1	2	2	2	2
A3 Green 1	3	3	3	3
A8 Red 2	4	4	4	4
A7 Yellow 2	5	5	5	5
A6 Green 2	6	6	6	6
A11 Red 3	7	7	7	7
A10 Yellow 3	8	8	8	8
A9 Green 3	9	9	9	9
A14 Red 4	10	10	10	10
A13 Yellow 4	11	11	11	11
A12 Green 4	12	12	12	12
B5 Red 5	13	13	13	13
B4 Yellow 5	14	14	14	14
B3 Green 5	15	15	15	15
B8 Red 6	16	16	16	16
B7 Yellow 6	17	17	17	17
B6 Green 6	18	18	18	18
B11 Red 7	19	19	19	19
B10 Yellow 7	20	20	20	20
B9 Green 7	21	21	21	21
B14 Red 8	22	22	22	22
B13 Yellow 8	23	23	23	23
B12 Green 8	24	24	24	24
C5 Red 9	25	25	25	25
C3 Green 9	26	26	26	26
C8 Red 10	27	27	27	27
C6 Green 10	28	28	28	28
C11 Red 11	29	29	29	29
C9 Green 11	30	30	30	30
C14 Red 12	31	31	31	31
C12 Green 12	32	32	32	32



Phase diagrams

Signal groups	1	5	10	2	6	9
Vehicle/Ped groups	Vg 1	Vg 5	Pg 2	Vg 2	Vg 6	Pg 1
Detector input						
Call						
Extend						
Increment						
Special Conditions	D0 demands on det 13 & 4. If only 13 or 4 demands, then call D10 or D20. If gap occurs in D0 then call D10 or D20. If no gap occurs in D0 then D0 terminated by max. If gap occurs in D10 or D20 & demands on det 15,16 or det 5,6 overlap SG1 or SG2 to A0. Else terminate D0.					

Detector Table

Det. inputs	Detector, or Loop and loop config.	Conr. term.	Patch card Input	Patch card Output	Det. mode (see note 3)	Detune Y/N
1	Lp1-4a(152)	P1	LDU1	CPU 1	Pres	N
2	Lp2-76µH	P2	LDU2	CPU 2	Pres	N
3	Lp3-76µH	P3	LDU3	CPU 3	Pres	N
4	Lp4-4a(152)	P4	LDU4	CPU 4	Pres	N
5	Lp5-107µH	P5	LDU5	CPU 5	Pres	N
6	Lp6-107µH	P6	LDU6	CPU 6	Pres	N
7	Lp7-1b(174)	Q7	LDU7	CPU 7	Pres	N
8	Lp8-4b(174)	Q8	LDU8	CPU 8	Pres	N
9	Lp9-128µH	Q9	LDU9	CPU 9	Pres	N
10	Lp10-128µH	Q10	LDU10	CPU 10	Pres	N
11	Lp11-128µH	Q11	LDU11	CPU 11	Pres	N
12	Lp12-1c(194)	Q12	LDU12	CPU 12	Pres	N
13	Lp13-3g(269)	R13	LDU13	CPU 13	Pres	N
14	Lp14-1d(213)	R14	LDU14	CPU 14	Pres	N
15	Lp15-113.3µH	R15	LDU15	CPU 15	Pres	N
16	Lp16-113.3µH	R16	LDU16	CPU 16	Pres	N

THIS DRAWING SUPERSEDES DRAWING No. 218439(C).

- Notes
- For further information on circuit refer to Philips 'PSC Housing wiring 'C' cabinet.' Philips drawing no. 9584 B11 21370-21380-21390.
  - 240V supply is for audiotactile units and/or external detectors if required.
  - Hold time for all detector channels to be set to 10 minutes (Philips) & 16 minutes (AWA).
  - For Loop Configurations refer Standard Drawing 1426.
  - Loops shown with a hash (#) are for traffic counting purposes only.
  - Cable runs only are shown on this drawing - for ducting and pit details refer to Design Layout drawing.

Revisions

Checked	Certified	Approved	Microfiled	Associated job nos	Dimensions in metres except where shown otherwise
///	///	///	///	272506 - 272507	0 2 4 6 8 10m

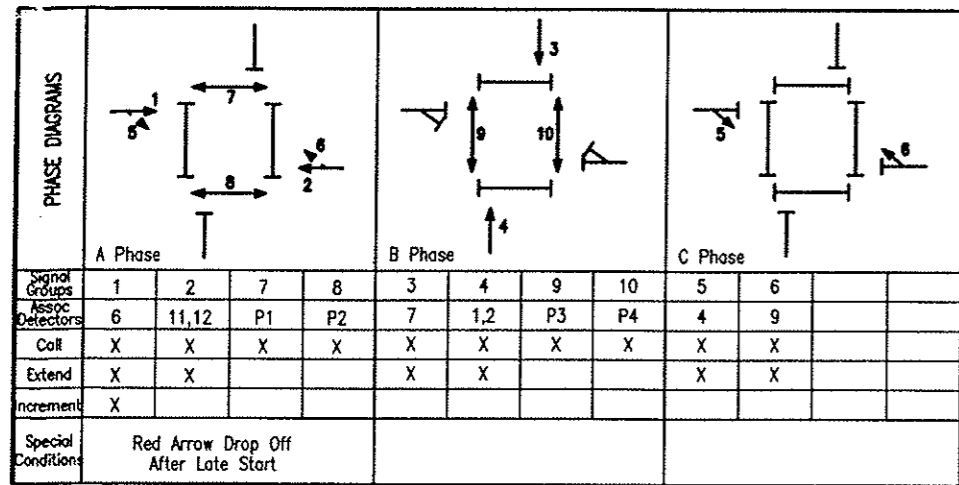
GLADSTONE CITY  
GLADSTONE - MT. LARCOM ROAD  
INTERSECTION OF GLENLYON RD. AND BRAMSTON ST.

TRAFFIC SIGNAL INSTALLATION  
PHILIPS PSC 2000 TYPE 'C' CABINET (IR)  
CABLE CONNECTIONS

Main Roads  
JOB No. 161/181/201  
No. 2 of 2 dwgs  
Drawing No. A

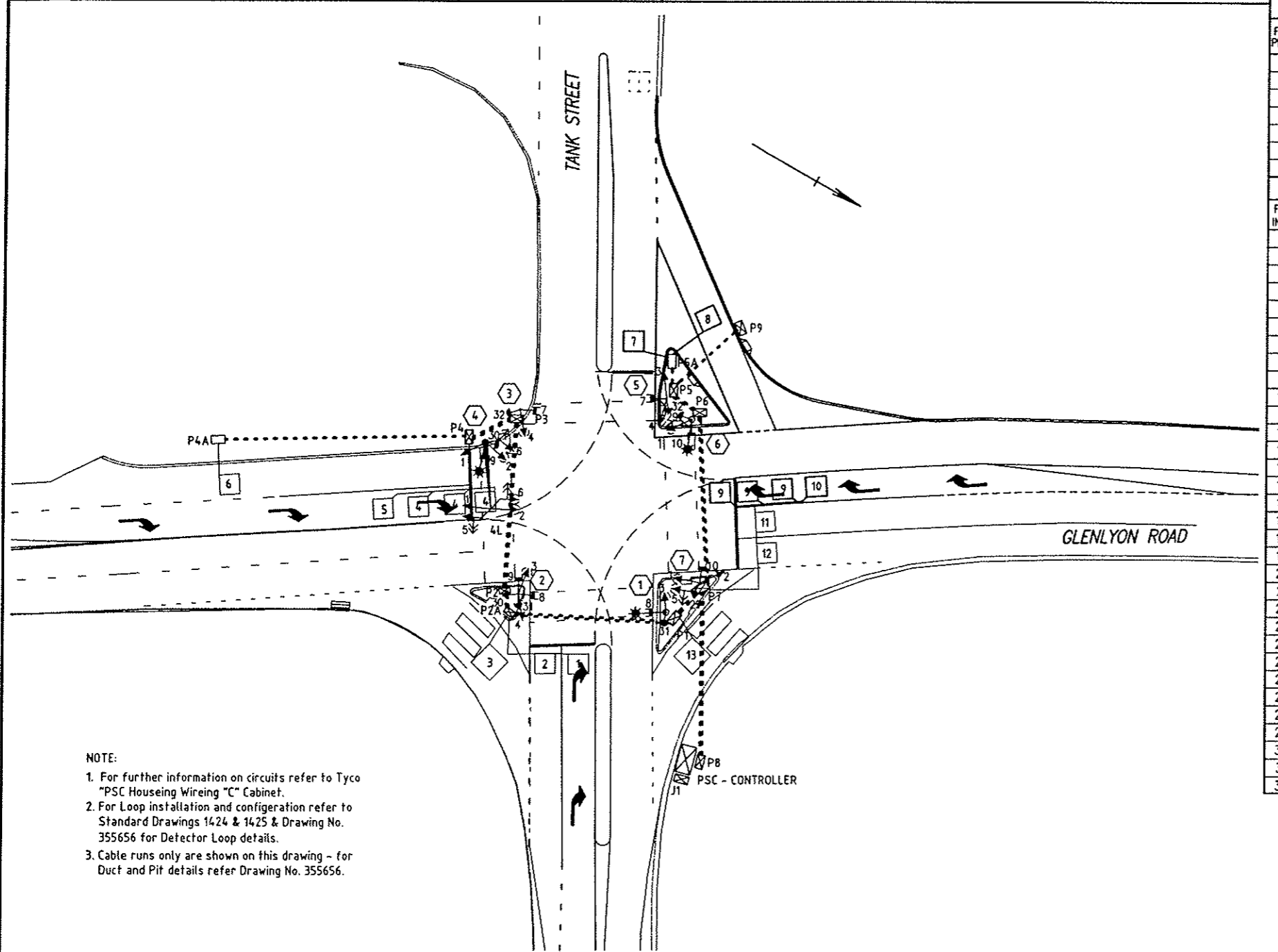
Site No. 4606  
ENGINEERING & TRAFFIC DESIGN  
Transport Technology Division  
CAD File: PSC272507

EA2	240V				
EA5	Ext det 1	17	17		12
EA6	Ext det 2	18	18		20
EA7	Ext det 3	21	21		21
EA8	Ext det 4	15	15		15
EA3	Det. comm.	26	26	26	26
EA1	Neutral	NI	Bk	NI	Bk
	Spare cores	19-25	Gy	16-25	Gy
	Cable size	29	29	29	29



**CONFLICT TABLE (X indicates conflict)**

Signal Groups	Signal Groups												Ped groups				
	1	2	3	4	5	6	7	8	9	10	11	12	7	8	9	10	
1		X	X	X										X	X	X	
2			X	X	X											X	X
3				X	X	X										X	X
4					X	X	X									X	X
5						X	X	X								X	X
6							X	X	X					X	X	X	
7								X	X								X
8									X	X							
9										X	X						
10											X	X					
11												X	X				
12													X	X			



**VEHICLE CLEARANCE TIMES**

FROM PHASE	YELLOW TIMES (SEC)	ALL RED TIMES (SEC)						
		A	B	C	D	E	F	G
A	4		2	2				
B	4	2		2				
C	4	2	2					
D								
E								
F								
G								

**DETECTORS**

FIELD INPUT	LOOP / P/BUTTON	CONFIGURATION	CABLE	CONTR TERM	LOGIC INPUT
1	Lp1	Existing		P1	1
2	Lp2	Existing		P2	2
3	Lp3	Existing		P3	3
4	Lp4	Existing		P4	4
5	Lp5	Existing		P5	5
6	Lp6	Existing		P6	6
7	Lp7	Existing		P7	7
8	Lp8	Existing		P8	8
9	Lp9	Existing		P9	9
10	Lp10	Existing		Q10	10
11	Lp11	Existing		Q11	11
12	Lp12	Existing		Q12	12
13	Lp13	Existing		Q13	13
14				14	
15				15	
16				16	
17				17	
18				18	
19				19	
20				20	
21				21	
22				22	
23				23	
24				24	
25				25	
26				26	
27				27	
28				28	
29	P/B 4	Audio		29	
30	P/B 3			30	
31	P/B 2			31	
32	P/B 1			32	

**NOTES**

- Clearance times calculated for 60km/hr.
- For traffic signal symbols see STD DWG 1436 (7/97)

Site No. 4605

Revisions	Certified	Date	Microfiled	Associated job nos	Dimensions in metres except where shown otherwise. Culvert sizes in millimetres.	Survey books
Original issue						

**GLADSTONE CITY (GLADSTONE TO MT LARCOM)**

CTL CHGE 2720m - 2850m

Reference Points: Preceding RPC, Dist. to start of job (km), From start to end of job, From end to following RPC, Following RPC

Survey: Bkds (Ckd, Ckd), Drawn NRS (Ckd, JDC), Design NRS (Ckd, JDC), Examined, Certified (RPEQ), Approved (District Director Penedo)

**TRAFFIC SIGNAL INSTALLATION**

PHILIPS PSC QC8-ID CONTROLLER

CABLE CONNECTIONS

Contract No. 161/181/12

**Queensland Government**  
Department of Main Roads

JOB No. 161/181/12

Drawing No. 355657

Contract No. / /

CAD REF: REC406-001-C-DWG-007

## **Appendix B. Base Year Validation**





TURN SUMMARY - AM

Location	Approach	Mvmt	ID	Count	Seed Values					Avg	St Dev	GEH
					560	28	7771	86524	2849			
Dawson Hwy/Phillip St	North	L	3c:3ba:3bb:3	200	189	185	197	195	194	192	5	0.559431
		T	3c:3ba:3bc:22	386	382	377	391	370	374	379	8	0.374833
		R	3c:3ba:3bd:3f	52	54	57	49	50	61	54	5	0.296481
		U	3c:3ba:3ba:3c	3	0	0	0	0	0	0	0	2.44949
	East	L	3:3bb:3bc:22	384	412	388	406	412	398	403	10	0.967773
		T	3:3bb:3bd:3f	83	88	72	86	91	87	85	7	0.196513
		R	3:3bb:3ba:3c	210	225	222	218	200	203	214	11	0.281221
		U	3:3bb:3bb:3	26	23	27	21	30	24	25	4	0.19803
	South	L	22:3bc:3bd:3f	87	77	78	89	93	83	84	7	0.324443
		T	22:3bc:3ba:3c	1,138	1132	1136	1115	1152	1143	1136	14	0.060434
		R	22:3bc:3bb:3	491	482	489	491	475	486	485	6	0.271504
		U	22:3bc:3bc:22	0	0	0	0	0	0	0	0	0
	West	L	3f:3bd:3ba:3c	63	60	48	53	64	60	57	6	0.756069
		T	3f:3bd:3bb:3	46	32	41	44	44	45	41	5	0.66411
		R	3f:3bd:3bc:22	30	31	36	23	29	24	29	5	0.258639
U		3f:3bd:3bd:3f	0	0	0	0	0	0	0	0	0	
Phillip St/Shoppin g Centre	North	L	10:8:7	25	23	18	24	27	29	24	4	0.161296
		R	10:8:3	25	30	30	13	29	28	26	7	0.19803
	East	T	3:8:7	678	677	695	696	710	704	696	12	0.720735
	West	L	3:8:10	44	49	47	57	34	44	46	8	0.327593
		T	3:8:7	718	677	695	696	710	704	696	12	0.812237

**TURN SUMMARY - PM**

Location	Approach	Mvmt	ID	Count	Seed Values					Avg	St Dev	GEH
					560	28	7771	86524	2849			
Dawson Hwy/Phillip St	North	L	3c:3ba:3bb:3	491	510	455	474	449	520	482	32	0.404778
		T	3c:3ba:3bc:22	862	838	854	894	892	869	869	24	0.250413
		R	3c:3ba:3bd:3f	103	109	99	104	125	107	109	10	0.519936
		U	3c:3ba:3ba:3c	4	0	0	0	0	0	0	0	2.828427
	East	L	3:3bb:3bc:22	594	619	605	626	642	568	612	28	0.733017
		T	3:3bb:3bd:3f	115	110	120	125	121	101	115	10	0.037268
		R	3:3bb:3ba:3c	153	152	153	141	154	142	148	6	0.390646
		U	3:3bb:3bb:3	75	64	66	71	65	78	69	6	0.731185
	South	L	22:3bc:3bd:3f	89	91	74	87	82	84	84	6	0.581284
		T	22:3bc:3ba:3c	606	563	553	614	644	635	602	42	0.183721
		R	22:3bc:3bb:3	269	292	297	277	260	268	279	16	0.573208
		U	22:3bc:3bc:22	0	0	0	0	0	0	0	0	0
West	L	3f:3bd:3ba:3c	143	136	147	132	134	152	140	9	0.276029	
	T	3f:3bd:3bb:3	60	61	55	66	59	57	60	4	0.073035	
	R	3f:3bd:3bc:22	162	150	167	173	172	137	160	16	0.173438	
	U	3f:3bd:3bd:3f	0	0	0	0	0	0	0	0	0	
Phillip St/Shopping Centre	North	L	10:8:7	135	161	142	142	149	158	150	9	1.289166
		R	10:8:3	101	90	102	112	107	95	101	9	0.019891
	East	T	3:8:7	836	898	841	855	805	888	857	37	0.728626
	West	L	3:8:10	34	26	30	32	27	34	30	3	0.743625
		T	3:8:7	861	898	841	855	805	888	857	37	0.122816



# Appendix C. Paramics Video Files